

## Enhancement of Effective Electromechanical Coupling Factor by Mass Loading in Layered SAW Device Structures

層構造 SAW デバイスの実効電気機械結合係数に及ぼす電極膜厚の影響

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### 1. Introduction

The effective electromechanical coupling factor  $K_e^2$  is a key parameter to determine the realizable filter bandwidth. Recently, Scandium-doped AlN (ScAlN) films have drawn much attention due to the strong piezoelectricity<sup>1-3</sup>. The authors reported that large SAW velocity  $V$ , small propagation attenuation, and large  $K_e^2$  of about 6.1% are simultaneously achievable when the film is combined with a high velocity base substrate such as single crystal diamond (SCD) and 6H-SiC for the Sezawa mode even for operation in the 3 GHz range<sup>2,3</sup>.

In many cases,  $K_e^2$  of the SAW is much lower than that of the bulk wave even when the same piezoelectric material is chosen. This is because the SAW field distribution does not match well to the electric field generated by the interdigital transducer (IDT), and thus  $K_e^2$  can be sometimes enhanced when heavy electrodes are used and/or the IDT is inlaid in the layered substrate.

This effect is well known also for the bulk acoustic wave (BAW) devices<sup>4</sup>, and is widely used in practical device design.

This paper describes drastic enhancement of  $K_e^2$  by mass loading in layered SAW device structures such as the Cu IDT/ScAlN film/Si substrate structure, and existence of this phenomenon is verified experimentally.

### 2. Simulation

SAW properties on the Cu electrode/Sc<sub>0.43</sub>Al<sub>0.57</sub>N film/Si structure were analyzed by the software SYNCL<sup>5</sup>, which calculates the input admittance of the infinitely long IDT on the structure as a function of the driving frequency  $f$ . The Sc<sub>0.43</sub>Al<sub>0.57</sub>N film thickness is set at  $0.5\lambda$ , where  $\lambda$  is the SAW wavelength. This thickness gives the maximum  $K_e^2$  when the Cu electrode thickness  $h_{Cu}$  is zero.

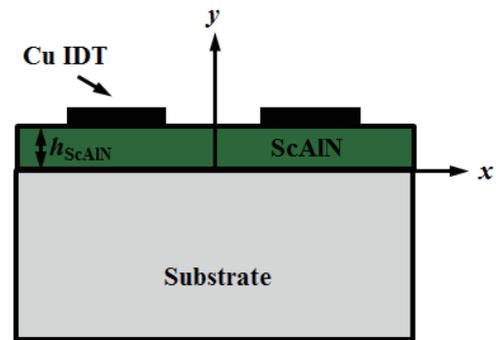


Fig. 1. Model structure used for simulation

Fig. 2 shows effective SAW velocity  $V$  and  $K_e^2$  as a function of  $h_{Cu}/\lambda$ . These values were estimated using the following formulas:

$$V = \lambda f_r \quad (1)$$

and

$$K_e^2 = (\pi f_r / 2 f_a) / \tan(\pi f_r / 2 f_a), \quad (2)$$

respectively, where  $f_r$  and  $f_a$  are the resonance and anti-resonance frequencies.

It is seen that  $V$  decreases monotonically with  $h_{Cu}/\lambda$  for the fundamental and second modes. On the other hand,  $K_e^2$  for the Sezawa mode increases with  $h_{Cu}/\lambda$ , and takes a maximum value of 9.1% at  $h_{Cu}/\lambda \sim 0.15$ , which is more than three times larger than the value when  $h_{Cu}/\lambda \sim 0$ . In contrast,  $K_e^2$  for the Rayleigh mode decreases with  $h_{Cu}/\lambda$ . This enhancement is caused by variation of the SAW field distribution to fit with the electric field excited by the IDT. Such  $K_e^2$  enhancement also occurs in SAWs on semi-infinite piezoelectric substrates<sup>6</sup>. But it is more prominent for the present case because only the limited region, i.e., piezoelectric film, is responsible for the wave excitation.

This phenomenon occurs in various layered SAW structures. More calculations can be found in Ref. 7.

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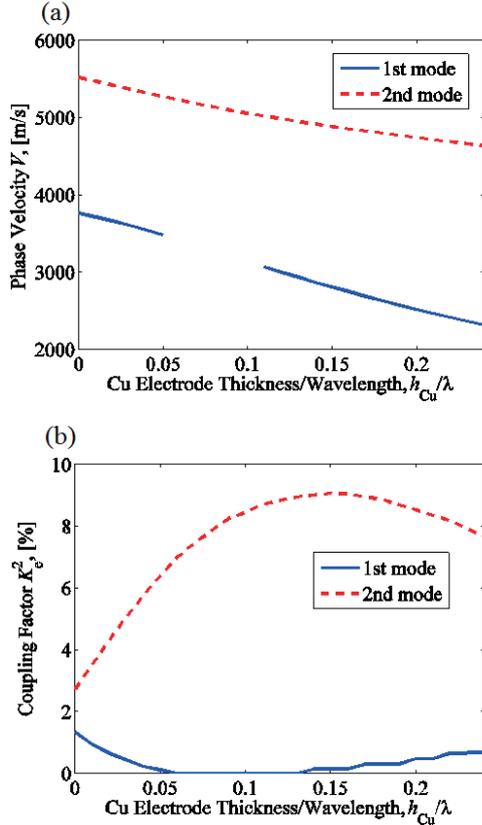


Fig.2. SAW properties on the ScAlN/Si structure when the mass loading is taken into account. (a) Variation of  $V$  with  $h_{Cu}/\lambda$ , (b) Variation of  $K_e^2$  with  $h_{Cu}/\lambda$

### 3. Experiment

For experimental verification of this phenomenon, a series of one port SAW devices were on the ScAlN film/Si substrate structure<sup>8)</sup>, and  $K_e^2$  was evaluated using Eq. (2). The device parameters are given in Table I. The Sc content  $r$  estimated by the X-ray fluorescence spectrometry was circa 22%.

Table I. Design parameters

ScAlN thickness, $h_{ScAlN}$	1.6 $\mu\text{m}$
Wavelength, $\lambda$	2, 2.2, 2.4 $\mu\text{m}$
Finger width, $w$	0.5 $\mu\text{m}$
Aperture, $W$	40 $\mu\text{m}$
Numb. of IDT finger pairs	80
Numb. of Reflector fingers	80
Cu electrode thickness, $h_{Cu}$	20, 100, 200 nm

Fig. 3 shows variation of  $K_e^2$  of the second mode with  $h_{Cu}$ . It is seen that  $K_e^2$  increases monotonically with  $h_{Cu}$ , and  $K_e^2$  is about 2% when  $h_{Cu}/\lambda \sim 0.1$ . The value is about three times larger than that when

$h_{Cu}/\lambda \sim 0.01$ . But the value is much smaller than that shown in Fig. 2(b). This is because of low  $r$  in the used ScAlN film. It results in not only reduction of the piezoelectricity but increase of the SAW velocity. Larger  $V$  tends to increase the Cu thickness giving maximum  $K_e^2$ . For example, the Cu thickness of 0.6  $\lambda$  is necessary for the AlN/Si structure.

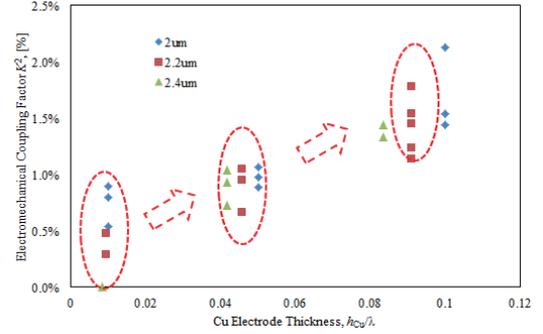


Fig.3.  $K_e^2$  on the ScAlN/Si structure changing with  $h_{Cu}/\lambda$

### 4. Conclusion

This paper describes drastic enhancement of  $K_e^2$  by mass loading in layered SAW device structures.

It is quite interesting about the SAW characteristics on high Sc content Cu IDT/ScAlN film/Si substrate structure.

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